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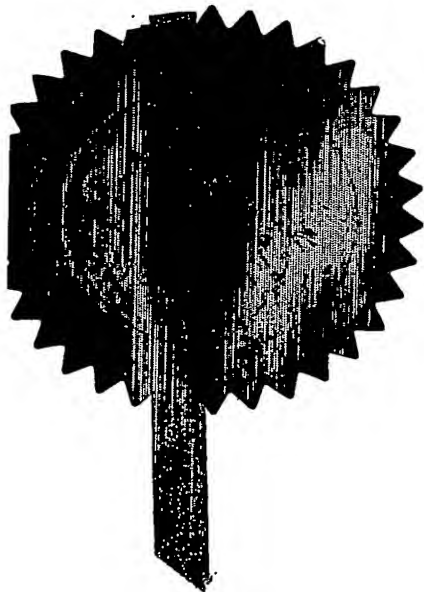
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The Patent Office

Cardiff Road
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1. Your reference

P32366-/LBA/RDE/GMU

2. Patent application number

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0306075.3

3. Full name, address and postcode of the or of each applicant (underline all surnames)

Renewable Devices Ltd
SAC Bush Estate
Edinburgh
EH26 0HP
United Kingdom

Patents ADP number (if you know it)

If the applicant is a corporate body, give the country/state of its incorporation

8589483001
United Kingdom

4. Title of the invention

Wind Turbine

5. Name of your agent (if you have one)

Murgitroyd & Company

"Address for service" in the United Kingdom to which all correspondence should be sent (including the postcode)

Scotland House
165-169 Scotland Street
Glasgow
G5 8PL

Patents ADP number (if you know it)

1198015

6. If you are declaring priority from one or more earlier patent applications, give the country and the date of filing of the or of each of these earlier applications and (if you know it) the or each application number

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Date of filing
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7. If this application is divided or otherwise derived from an earlier UK application, give the number and the filing date of the earlier application

Number of earlier application

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8. Is a statement of inventorship and of right to grant of a patent required in support of this request? (Answer 'Yes' if:

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- a) any applicant named in part 3 is not an inventor, or
 - b) there is an inventor who is not named as an applicant, or
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Claim(s)	-
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11. I/We request the grant of a patent on the basis of this application.

Signature *Graham Murnane* Date 17 March 2003
Murgitroyd & Company

12. Name and daytime telephone number of person to contact in the United Kingdom
- | | |
|----------------|---------------|
| GRAHAM MURNANE | 0141 307 8400 |
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1 Wind turbine

2

3 The invention relates to wind turbines, and more
4 particularly to a wind turbine for mounting on a
5 roof and for use with a domestic heating system.

6

7 Governments are committed to reduce CO₂ emissions
8 over the next few years. Along with energy
9 efficiency measures there has been an increased
10 emphasis on renewable sources of energy. Analysis
11 of energy demand shows that 6% of the UK's annual
12 energy demand is from domestic water heating and 12%
13 from domestic space heating. Use of wind turbine
14 technology could provide substantial economic
15 benefits to over 33% of UK households and could
16 reduce the UK's CO₂ emissions by as much as 2%.
17 Similar benefits are possible in other countries.

18

19 Existing micro wind turbines used to generate
20 domestic electricity require expensive intermediate
21 battery systems to compensate for the unregulated
22 and inconsistent supply of electricity produced.

1 Existing turbines of a size suitable for mounting on
2 a roof to provide domestic power are designed for
3 smooth airflow only and will oscillate violently
4 with the compressed and turbulent airflow found
5 over, and around, buildings creating noise and
6 inefficient generation.

7
8 It is an object of the present invention to overcome
9 one or more of the aforementioned problems.

10
11 According to a first aspect of the invention there
12 is provided a rotor for a wind turbine comprising a
13 plurality of radial blades and a ring-shaped
14 aerofoil diffuser connecting the outer tips of the
15 blades.

16
17 Preferably the aerofoil diffuser extends downstream
18 from the outer tips of the blades. The outer tips
19 of the blades may be connected to the diffuser at
20 the leading edge of the diffuser. Preferably the
21 aerofoil diffuser tapers radially outwards from the
22 outer tips of the blades to form a substantially
23 frusto-conical diffuser.

24
25 Preferably the blades are inclined at an angle
26 relative to a transverse rotor plane perpendicular
27 to the rotational axis of the rotor. The angle of
28 inclination may vary along the length of the blade.

29
30 Preferably the angle of inclination of each blade is
31 greater at an intermediate portion of the blade than
32 at the outer tip of the blade. Preferably the blade

1 is substantially parallel to the transverse rotor
2 plane at the outer tip of the blade.

3
4 According to a second aspect of the invention there
5 is provided a wind turbine comprising a rotor
6 according to the first aspect. Preferably the wind
7 turbine further comprises mounting means adapted to
8 allow rotation of the turbine and rotor about a
9 directional axis perpendicular to the rotational
10 axis. This allows the turbine to be oriented in the
11 optimum direction depending on wind conditions.

12
13 Preferably the wind turbine further comprises a
14 furling means adapted to rotate the rotor about the
15 directional axis so that the rotational axis is not
16 parallel to the direction of airflow when the
17 airflow speed is greater than a predetermined
18 airflow speed. Preferably the aerofoil diffuser is
19 adapted to divert radial airflow from the outer tips
20 of the blades to circumferential airflow during
21 furling when the rotational axis is not parallel to
22 the direction of airflow.

23
24 Preferably the furling means comprises a non-linear
25 furling means adapted to provide no furling over a
26 first lower range of airflow speed and a varying
27 degree of furling over a second higher range of
28 airflow speed. Preferably the furling means
29 comprises at least two tail fins extending
30 downstream of the diffuser. Preferably the furling
31 means comprises two tail fins provided diametrically
32 opposite each other, but more tail fins may be

1 provided if required, providing the positions of the
2 tail fins are balanced.

3
4 Preferably one of the tail fins is a moveable tail
5 fin hingedly mounted for rotation about a tangential
6 hinge line. The moveable tail fin may be mounted on
7 mounting boom and the hinge line may be provided at
8 the connection point of the mounting boom and the
9 nacelle, so that the mounting boom also rotates, or
10 at the connection between the mounting boom and the
11 moveable tail fin so that only the moveable tail fin
12 rotates.

13
14 Preferably the moveable tail fin is rotationally
15 biased by biasing means to an at-rest position in
16 which the leading edge of the moveable tail fin is
17 closer to the axis of rotation than the trailing
18 edge of the moveable tail fin, such that the
19 moveable tail fin is angled at an at-rest attack
20 angle to the axis of rotation. The biasing means
21 may be non-linear. Preferably the biasing means is
22 adapted to hold the moveable tail fin in the at-rest
23 position until the airflow speed reaches a
24 predetermined speed. Preferably, as the airflow
25 speed increases beyond the predetermined speed the
26 upstream fin rotates and the attack angle decreases.
27 This results in unbalanced aerodynamic loading on
28 the wind turbine, so that the wind turbine rotates
29 about its mounting axis to a furled position.

30

1 According to a third aspect of the present invention
2 there is provided a wind turbine heating system
3 comprising:

4 a wind turbine driven generator,
5 a first liquid storage vessel,
6 one or more electrical heating elements adapted
7 to heat liquid in said first vessel, and
8 control means adapted to control the supply of
9 electricity generated by said generator to said one
10 or more electrical heating elements.

11
12 Preferably the system comprises a wind turbine
13 according to a second aspect of the invention.

14
15 Preferably the first liquid storage vessel is a
16 domestic hot water tank and the liquid is water.

17
18 Preferably the system comprises a plurality of
19 electrical heating elements, and the control means
20 is adapted to supply electrical power to a
21 proportion of the electrical heating elements, the
22 proportion being dependent upon the instantaneous
23 electrical power generated by the generator.

24
25 The system may comprise a second liquid storage
26 vessel and one or more auxiliary electrical heating
27 elements adapted to heat liquid in said second
28 vessel. The control means may be adapted to supply
29 electrical power to said one or more auxiliary
30 electrical heating elements when the temperature of
31 the liquid in the first vessel reaches a
32 predetermined temperature. In one embodiment the

1 second liquid storage vessel is a domestic cold
2 water tank and the liquid is water. In another
3 embodiment the second liquid storage vessel is a
4 radiator.

5
6 Preferably the heating element in the first liquid
7 vessel is enclosed by means of a tube. This tube is
8 open on the underside thereof in order to allow
9 water to flow from beneath the tube towards the
10 heating element. The tube will enclose and extend
11 over in essence the entire length of the heating
12 element. The water near the heating element will be
13 heated and will flow upwards due to natural
14 convection. The presence of the tube will direct
15 the heated water towards a zone of the heated water.
16 The presence of the tube will enable the formation
17 of different and separate heat zones within the
18 first liquid storage vessel.

19
20 Preferably, the wind turbine heating system
21 according to the present invention is provided with
22 a control system in order to control the level of
23 power taken from the wind turbine. For efficiency
24 reasons the maximum power take-off from the wind
25 turbine is approximately 60%, as given by the Betz
26 limit. According to the present invention the
27 control system of the wind turbine will measure the
28 energy yield of the wind turbine in real time. The
29 control system is adapted to increase or decrease
30 the power take-off from the wind turbine by a small
31 amount. After a certain time period, the control
32 system will measure the energy yield of the wind

1 turbine again. The variation in the yield is
2 determined and the amount of power taken from the
3 wind turbine is again adjusted, depending on the
4 measured value for the yield. When the extra load
5 on the wind turbine causes the yield of the wind
6 turbine to increase the control system will increase
7 the load on the wind turbine further by a small
8 amount. Thereafter the yield of the wind turbine is
9 again measured in order to determine the effect of
10 the further increase of the load on the yield of the
11 turbine. If the increase of the load will result in
12 a decrease of the yield, the process is reversed.

13

14 According to a fourth aspect of the invention there
15 is provided a wind turbine according to the second
16 aspect comprising means for reducing the operating
17 vibrations caused by harmonic resonance within the
18 turbine, tower and mounting structure.

19

20 Preferably the wind turbine is provided with a
21 nacelle damping system. The nacelle damping system
22 according to the invention will help to isolate the
23 vibrations in the generator and turbine from the
24 tower.

25

26 Preferably the wind turbine is provided with
27 mounting brackets for mounting the turbine on a
28 surface, the brackets having a sandwich construction
29 of visco-elastic materials and structural materials.

30

31 The mounting means can be of any cross-sectional
32 shape, but is typically tubular. Preferably, the

1 tower contains one or more cores of flexible
2 material, such as rubber, with sections with a
3 reduced diameter, which are not in contact with the
4 tower's inner radial surface. These reduced
5 diameter sections alternate with normal sized
6 sections, which are in contact with the tower's
7 inner surface.

8
9 This serves to absorb vibrations in the tower
10 through the energy dissipated in the flexible core
11 before they reach the mounting brackets. The rubber
12 core thereby acts to force the system's resonant
13 frequency above the turbine driving frequency. By
14 altering the cross-sectional shape and length of
15 each of the reduced diameter sections, the system
16 can be "tuned" to remove a range of vibration
17 frequencies from the mounting structure.

18
19 The sandwich mounting bracket compliments the
20 mounting means core design and suppresses vibrations
21 that come from the nacelle. The nacelle itself
22 supports the generator through bushes designed to
23 eliminate the remaining frequencies. These three
24 systems act as a high/low pass filter where the only
25 frequencies that are not attenuated are those out-
26 with the operating range of the turbine.

27
28 An embodiment of the present invention will now be
29 described with reference to drawings wherein:

30
31 Fig 1 shows a schematic view of the wind turbine
32 according to the present invention;

1

2 Fig 2 shows a top view of the rotor and the furling
3 device of the wind turbine according to Fig 1;

4

5 Fig 3 shows in detail an embodiment of one boom of
6 the furling device according to the present
7 invention;

8

9 Fig 4 shows the connection of the boom according to
10 Fig 3 through the nacelle;

11

12 Fig 5 shows the connection of the tip of the boom
13 according to Fig 3 to the tail fin;

14

15 Fig 6 shows a schematic overview of a heating device
16 for heating water which is adapted to be coupled to
17 a wind turbine according to the present invention;

18

19 Fig 7 shows diagrammatically the working of the
20 control system of the heating device according to
21 Fig 6;

22

23 Figs 8 and 9 show a further embodiment of a heating
24 device for heating water, which is adapted to be
25 connected to the wind turbine according to the
26 present invention; and

27

28 Fig 10 shows a cross-sectional view of the mounting
29 means for the wind turbine according to the present
30 invention, wherein the interior is provided with a
31 vibration damping core.

32

1 Figs 11 and 12 show a cross-sectional view of the
2 mounting means according to Fig 10 as alternative
3 embodiments for the vibration damping core.
4

5 In Fig 1 a possible embodiment of the wind turbine
6 according to the present invention is shown. The
7 wind turbine comprises a rotor 20 having a core 25
8 and radial blades 30 extending from the core 25
9 towards the outer tip 31 of the blades 30. The
10 rotor comprises a radial aerofoil 21, attached to
11 and encircling the rotor blades 30. The rotor 20,
12 by means of the core 25, is rotationally fixed to a
13 nacelle 41. The rotor 20 is able to rotate about
14 the rotational axis 26. The nacelle 41 is
15 rotationally mounted on top of mounting means 40.
16 The mounting means 40 allow the wind turbine 10 to
17 be fixed on a support (not shown). The nacelle 41
18 moreover is provided with a furling mechanism 50.
19 The furling mechanism 50 comprises a first boom 51
20 and a second boom 52. The booms 51,52 and their
21 respective ends thereof are provided with tail fins
22 53,54.
23

24 The furling mechanism 50 has two functions. The
25 first function is to keep the rotational axis 26 of
26 the rotor 20 essentially parallel to the
27 momentaneous direction of the airflow. In Fig 1 the
28 airflow is schematically indicated by means of
29 arrows 15. The second function of the furling
30 device 50 is to rotate the rotor 20 out of the wind
31 when the wind velocity exceeds the output power
32 requirements of the wind turbine or endangers the

1 system's integrity, in order to protect the wind
2 turbine 10 against unacceptable high loads.

3

4 The construction and the working of the furling
5 mechanism will be clarified below, with reference to
6 Figs 2, 3, 4 and 5.

7

8 As shown in Fig 1, the radial aerofoil 21 is
9 attached to and encircles the turbine blades 30.
10 The radial aerofoil 21 will create a slight venturi
11 effect near the blade tips where the resulting
12 increase in air velocity has the largest effect.
13 This increases the overall efficiency of the turbine
14 10, which compensates for the slight increase in
15 weight and drag caused by the addition of the
16 aerofoil 21. The aerofoil will also create a more
17 laminar flow along the rotor blades. This is
18 important since the airflow on a roof typically is
19 turbulent. A further advantage is the fact that the
20 presence of the radial aerofoil 21 will increase the
21 mechanical strength of the rotor 20, allowing more
22 efficient aerofoil section to each blade 30.

23

24 In Fig 1 it can be seen that the design of the blade
25 30 is such that the outer tips 31 of the blade 30
26 are in essence perpendicular to the rotational axis
27 26.

28

29 The outer tips 31 of the blade are connected near
30 the leading edge 22 of the aerofoil 21. The number
31 of blades 30 may be varied.

32

1 In Fig 2 a top view is shown of the rotor 20 and the
2 furling device 50 of the wind turbine 10 according
3 to Fig 1. The furling device 50 comprises booms
4 51,52 each provided with a tail fin 53,54 at the end
5 thereof. The airflow 15 will exert a certain
6 pressure on the tail fins 53,54. The tail fins will
7 balance and stabilise the position of the rotor 20
8 with respect to the direction of the airflow 15.
9 When the direction of the airflow 15 changes the
10 resulting pressure on the tail fins 53,54 will also
11 change. The resulting force will cause the rotor 20
12 to rotate in order to maintain the direction of the
13 airflow 15 in essence in line with the rotational
14 axis 26 of the rotor 20. During normal furling the
15 presence of the aerofoil 21 will reduce vibrations
16 caused by imbalanced blade tip vortex shedding.
17 This is achieved in that the aerofoil will act to
18 divert the airflow from the blade tips during
19 furling.
20
21 The furling device 50 according to the present
22 invention not only maintains an optimal angle
23 between the rotor 20 and the airflow 15, but in
24 addition acts to protect the turbine 20 during
25 excessively high wind loadings. The furling device
26 50 is designed to rotate the turbine 20 out of the
27 airflow when the wind velocity exceeds the output
28 power requirements of the turbine or when the wind
29 loading compromises the integrity of the rotor 20.
30 As shown in Fig 2, the tail fins 53,54 form a wedge
31 pointing into, out of substantially parallel to the
32 wind. Excessive wind loadings will make the tail

1 fins 53,54 move and/or rotate with respect to the
2 nacelle 41. Preferably one of the fins has no
3 travel or limited travel, causing the rotor 20 to
4 furl as the second fin continues to rotate under
5 high airflow velocities. It means that the furling
6 mechanism 50 according to the present invention
7 under moderate wind velocity will keep the rotor 20
8 in a stable condition and at a preferred angle with
9 respect to the airflow 15. Only after exceeding a
10 predetermined wind velocity, the same furling device
11 50 will cause the rotor 20 to rotate out of the wind
12 in order to protect the integrity thereof.

13

14 The construction of the furling device 50 according
15 to the present invention causes the furling device
16 to act non-linearly in relation to the wind
17 velocity. The furling device 50 limits the
18 turbine's susceptibility to gusts and turbulence.
19 Light gusts will not be able to move the rotor out
20 of the wind. The safety function of the furling
21 device 50 will only operate in high wind situations
22 in order to protect the turbine and a respective
23 generator.

24

25 As shown in Fig 2 the booms 51 and 52 extend from
26 the nacelle to the tail fins, in the downwind
27 direction of the rotor 20. The respective tail fins
28 53 and 54 are positioned essentially in line with
29 the exterior dimensions of the rotor 20. The
30 construction of the furling device 50 according to
31 the present invention enables a compact construction
32 and does not necessitate free space behind the

1 nacelle 41. That means that the design of this
2 furling system allows the overall length of the
3 turbine to be considerably reduced when compared to
4 existing wind turbines.

5
6 In Figs 3 and 4 the first embodiment of the boom 51
7 and respective tail fin 53 is shown. The arrows
8 indicate the movement of the boom 51 with respect to
9 the nacelle 41. The angle between the rotation axis
10 26 of the rotor (not shown) and the tail fin 53 is
11 changed by use of a hinge 60 located at the base of
12 the boom 51. As shown in Fig 4, the boom 51 is held
13 at a fixed angle to axis 26 by a coil spring 61.
14 When the wind loading on the fin 53 is sufficiently
15 large, the boom 51 and the fin 53 rotate against the
16 retaining force of the coil spring 61, causing an
17 out of balance aerodynamic loading on the rotor 20.
18 This out of balance force will cause the nacelle to
19 rotate about its mounting axis 42 (see Fig 1). It
20 should be noted that the coil spring 61 as shown in
21 Fig 4 is simply for explanatory purposes and any
22 type of spring could be used in the hinge 60.

23
24 In Fig 5 an alternative embodiment is shown wherein
25 the rotation of the furling fin takes place about a
26 hinge 70 located at the outer tip of the boom. As
27 shown in Fig 5 clockwise rotation of the fin 53 at
28 the hinge 70 is limited by an end stop 71. The
29 anti-clockwise rotation of the fin 53 is restrained
30 by the reaction of a coil spring (not shown). When
31 the speed of the airflow 15 increases to a level at
32 which furling is required, the retaining force of

1 the spring in the hinge 70 is overcome and the fin
2 53 will rotate. This causes an out of balance
3 aerodynamic loading on the rotor. This out of
4 balance force will again cause the nacelle to rotate
5 about its mounting axis 42, until the aerodynamic
6 forces on the turbine are in equilibrium. The non-
7 linear furling mechanism 50 according to the present
8 invention will keep the turbine windward and stable
9 until the wind velocity compromises the systems
10 safety and the turbine is progressively yawed from
11 the wind. The furling device 50 therefore reduces
12 constant yawing of the turbine during gusts, which
13 would otherwise create unwanted oscillations and
14 turbine blade noise.

15

16 The actual furling angle necessary to protect the
17 wind turbine can be limited because of the presence
18 of the aerofoil 21. A certain furling of the rotor
19 20 will result in aerodynamic stalling along the
20 foil 21. As soon as the stalling starts, the power
21 of the wind flow 15 on the rotor 20 will drop.

22

23 In Fig 6 a schematic overview of a wind turbine
24 heating system is shown. The wind turbine heating
25 system comprises a first water reservoir 118. In
26 the water reservoir one or more electric heating
27 elements 114 are provided. The electrical heating
28 elements 114 are coupled with the wind turbine 10
29 via a control unit 116. The electrical current
30 generated by the wind turbine 10 will be directed to
31 the electrical heating elements 114 in order to heat
32 up the water contained in reservoir 118. While the

1 efficiency of the heat transfer for electric heating
2 elements may be considered to be near 100%,
3 operating an element at a lower power input than
4 that for which it was designed results in a lower
5 element temperature. The nature of wind power is
6 such that the power output will usually be
7 considerably below the overall rated power of the
8 heating system. As such, it is necessary to use
9 heating elements 114 with an appropriate power
10 rating.

11
12 The water reservoir 118 is designed to store warm
13 water, prior to use. The reservoir 118 may be a
14 cylinder manufactured from copper alloy, though
15 enamelled steels and plastic may also be used.
16 Steel cylinders are better suited to higher pressure
17 applications, while copper is attractive due to its
18 inherent corrosion resistance and the associated
19 long service-life. For vented systems and their
20 associated lower cylinder pressure, copper cylinders
21 are well suited.

22
23 When, using the system according to Fig 6, all of
24 the water in the reservoir 118 has been heated to
25 the maximum allowable temperature, the control unit
26 116 will no longer allow the heating elements 114 to
27 dissipate power into the water reservoir 118. That
28 means that the power generated by the wind turbine
29 has to be "dumped" elsewhere. As long as the wind
30 turbine 10 is generating electricity, it is
31 essential that there is a means of dissipating the
32 electrical energy at all times.

1 This is done by using a heating element 115 immersed
2 in water. This can be installed to preheat the
3 water in a cold water reservoir 120. If the volume
4 of the cold water cistern is in the region of 200-
5 300 litres, as is typical of a small house, then
6 this would be sufficient to dissipate any quantity
7 of excess power. If the reservoir 120 were not
8 insulated then much of the heat energy would be lost
9 to the surroundings in any case. The frequency with
10 which the dump load would be utilised should be
11 sufficiently small that there would be no
12 economically feasible means of utilising the excess
13 power. Excess power from the wind turbine could
14 also be directed to a building space-heating system,
15 or used to pre-heat a cold water feed to a boiler or
16 similar water heating equipment.

17
18 Water heated in a hot water reservoir 118 with
19 elements 114 will tend to form stratified layers.
20 The temperature within each layer will not vary much
21 as heat will be spread by conduction and convection.
22 A high temperature gradient exists between layers.
23 Heat transfer by conduction is very low in water.
24 This phenomenon would be useful in a situation where
25 several heating elements are used, as the top layer
26 could be heated up, and then left undisturbed by the
27 convection below it as lower layers were
28 subsequently heated.

29
30 It should be noted that the heating element design
31 described herein could be used with or without a
32 mains connection in tandem. The mains connection

1 would allow the immersion heating element (or a
2 dedicated mains element) to provide energy when none
3 is available from the wind turbine.

4
5 Typically the rated power of the heating system
6 according to Fig 6 could be in the range of about 3
7 kW.

8
9 With respect to the efficiency of the wind turbine,
10 the power extracted from the wind by the rotor
11 should be limited to approximately 60% (59,6%).
12 Because of the fact that the wind turbine according
13 to the present invention will be operated in mainly
14 turbulent airflows, the efficiency of the wind
15 turbine according to the present invention can be
16 improved by adding a new control system.

17
18 Fig 7 schematically shows the working of the control
19 system according to the present invention. First,
20 the load on the wind turbine is near a predetermined
21 starting level (L0). The control system will
22 measure the corresponding yields of the wind
23 turbine. Thereafter the load on the wind turbine is
24 increased or decreased by a small amount. In the
25 example of Fig 7 the load on the wind turbine is
26 decreased. Thereafter the control system measures
27 the new yield level of the wind turbine. If the
28 yield is found, the same procedure is repeated.
29 That means that as long as the yield increases the
30 load will be decreased. As soon as a further
31 decrease of the load will result in a decrease of
32 the yield, the process is reversed. That means that

1 then the load on the wind turbine will be increased
2 and the corresponding effect on the yield will be
3 monitored.

4
5 Because of the fact that the wind velocity on the
6 rotor will be continuously alternating, the time
7 interval for increasing and decreasing the amount of
8 load on the wind turbine will typically be in the
9 range of several microseconds.

10
11 The efficiency of the wind turbine heating system
12 can be further increased when using an alternative
13 water reservoir 120 as shown in Fig 8. The water
14 reservoir 119 is provided with an electrical heating
15 element 124. The heating element 124 is covered,
16 over a substantive length thereof, by means of an
17 enclosing tube 125. The bottom end 126 of the tube
18 125 is open. This enables water to flow in between
19 the exterior of the heating device 124 and the
20 interior of the tube 125. As soon as current passes
21 through the element 124 the electrical energy will
22 be converted into heat energy and this heat energy
23 is then transferred to the water. The water film
24 directly enclosing the heating element 124 will be
25 heated and, due to natural convection, will flow
26 towards the top of the reservoir 128 and is
27 prevented from diffusing radially into the reservoir
28 128. Because of the presence of the tube 125 the
29 heated water is directed towards a warm water zone
30 130 in a top part of the reservoir 128. The heat
31 generated by the heating element 124 therefore is
32 concentrated in the top part of the reservoir 128

1 and is prevented from diffusing radially into the
2 reservoir 128. This will limit the time necessary
3 to heat up water to a preferred temperature thus
4 reducing the energy consumption of thereof.

5
6 As soon as the power generated by the wind turbine
7 is increased, the amount of heat transferred to the
8 water in the reservoir 128 is also increased. This
9 means that the flow of heated water towards the top
10 part of the reservoir 128 will increase, resulting
11 in mixing the thermally stratified layers, and in an
12 enlarged warm water area 130. This effect is shown
13 in Fig 9. Because of the construction of the
14 reservoir 128, power no longer has to be "dumped".
15 The use of the reservoir 128 is especially suitable
16 for a wind turbine, because of the fact that the
17 nature of wind power is such that the power output
18 will usually fluctuate and moreover will be below
19 the overall rated power of the heating system.

20
21 During normal operation of a wind turbine according
22 to the invention, vibrations are caused by harmonic
23 resonance within the turbine, tower and mounting
24 structure. These come from blade imbalances, due to
25 deformation during operation or bearing vibration in
26 the generator and turbine hub. Eliminating
27 resonance in micro-wind turbines is especially
28 difficult as they operate through a wide
29 range of turbine tip-speeds. The design described
30 below reduces the operating vibrations by
31 controlling the turbine tip-speeds so that they

1 remain outside natural resonant frequencies, and
2 through novel vibration absorption measures.
3 Mounting a horizontal axis wind turbine on a
4 building structure requires the damping of critical
5 frequencies and the moving of harmonics beyond the
6 system operating frequencies. The damping system on
7 the rooftop wind turbine is integrated into the
8 design of the mounting means and nacelle of the
9 turbine. These vibration absorbing systems work
10 together to create a silent running rooftop turbine.
11
12 The novel wind turbine mounting bracket uses a
13 sandwich construction of viscoelastic materials and
14 structural materials.
15
16 The mounting means tower contains an innovative
17 core, typically of rubber, which has some sections
18 which have a reduced cross-sectional area and are
19 not in contact with the mounting means' inner
20 surface and some sections which are. This serves to
21 absorb vibrations in the mounting means through the
22 energy dissipated in the rubber core before they
23 reach the mounting bracket. The rubber core also
24 acts to force the system's resonant frequency above
25 the turbine driving frequency.
26
27 In Fig 10 a possible embodiment of the interior of
28 the mounting means is shown, in cross-section. In
29 this embodiment, the mounting means is tubular in
30 cross-section. The mounting means 40 comprises a
31 hollow core wherein a cylindrical core element 90 is
32 present. The core element 90 in the middle thereof

1 is provided with a hollow section 91 in order to
2 allow elements such as a power line to be guided
3 through the interior of the core element 90. The
4 core element 90 is provided with sections 92 with an
5 exterior diameter corresponding substantially to
6 the interior diameter of the mounting means 40.
7 These sections alternate with sections 93 that have
8 a reduced diameter and are not in contact with the
9 mounting means' 40 inner radial surface. The
10 sandwich mounting bracket together with the mounting
11 means core design suppresses vibrations in the
12 system. The main sources for those vibrations are
13 vibrations transmitted from the wind turbine to the
14 building, and the aerodynamic turbulence around
15 obstacles, which decreases power output but more
16 importantly shortens the working life of the wind
17 turbine.

18
19 In Fig. 11 an alternative embodiment of the interior
20 of the mounting means is shown, in cross-section.
21 The hollow core of the mounting means 40 is provided
22 with a core element 94. The core element 94 in the
23 middle thereof is provided with a hollow section 91.
24 The core element 94 is provided with sections 92
25 with an exterior diameter corresponding
26 substantially to the interior diameter of the
27 mounting means 40. These sections alternate with
28 sections 93 that have a reduced diameter and are not
29 in contact with the mounting means' 40 inner radial
30 surface. When comparing Figs 10 and 11 it will be
31 clear that the shape of the recesses in respective
32 core elements 90 and 94 differs. It should be noted

1 that Figs 10 and 11 are for illustration purposes
2 only. Alternative embodiments for the core elements
3 are also possible.

4
5 Fig 12 shows a further embodiment of the interior of
6 the mounting means 40. As shown in Fig 12, the
7 interior of the mounting means 40 comprises several
8 core elements 95, which are inserted in the mounting
9 means wherein a first element 95 abuts an adjacent
10 element 95. In the example of Fig 12 the shape of
11 the recesses in the respective elements 95 again
12 differs from the embodiments according to Fig 10 and
13 Fig 11.

14
15 In a wind turbine noise comes from two areas,
16 aerodynamic sources and mechanical sources.
17 Aerodynamic noise is radiated from the blades,
18 originating due to the interaction of the blade
19 surfaces with turbulence and natural atmospheric or
20 viscous flow in the boundary layer around the
21 blades. Mechanical noise is due to the relative
22 motion of mechanical components and the dynamic
23 response among them. This effect may be magnified
24 if the nacelle, rotor and tower transmit the
25 mechanical noise and radiate it, acting as a
26 loudspeaker. Two types of noise problem exist: air
27 borne noise which is noise which is transmitted
28 directly from the component surface or interior into
29 the air, and structure borne noise which is
30 transmitted through the structure before being
31 radiated by another component.

32

1 The turbine mounting and mounting means are designed
2 to push the resonant frequency of the whole
3 structure above the operation vibration frequencies
4 caused by blade unbalances and deformations. The
5 mounting contains a damping system which eliminates
6 vibrations.

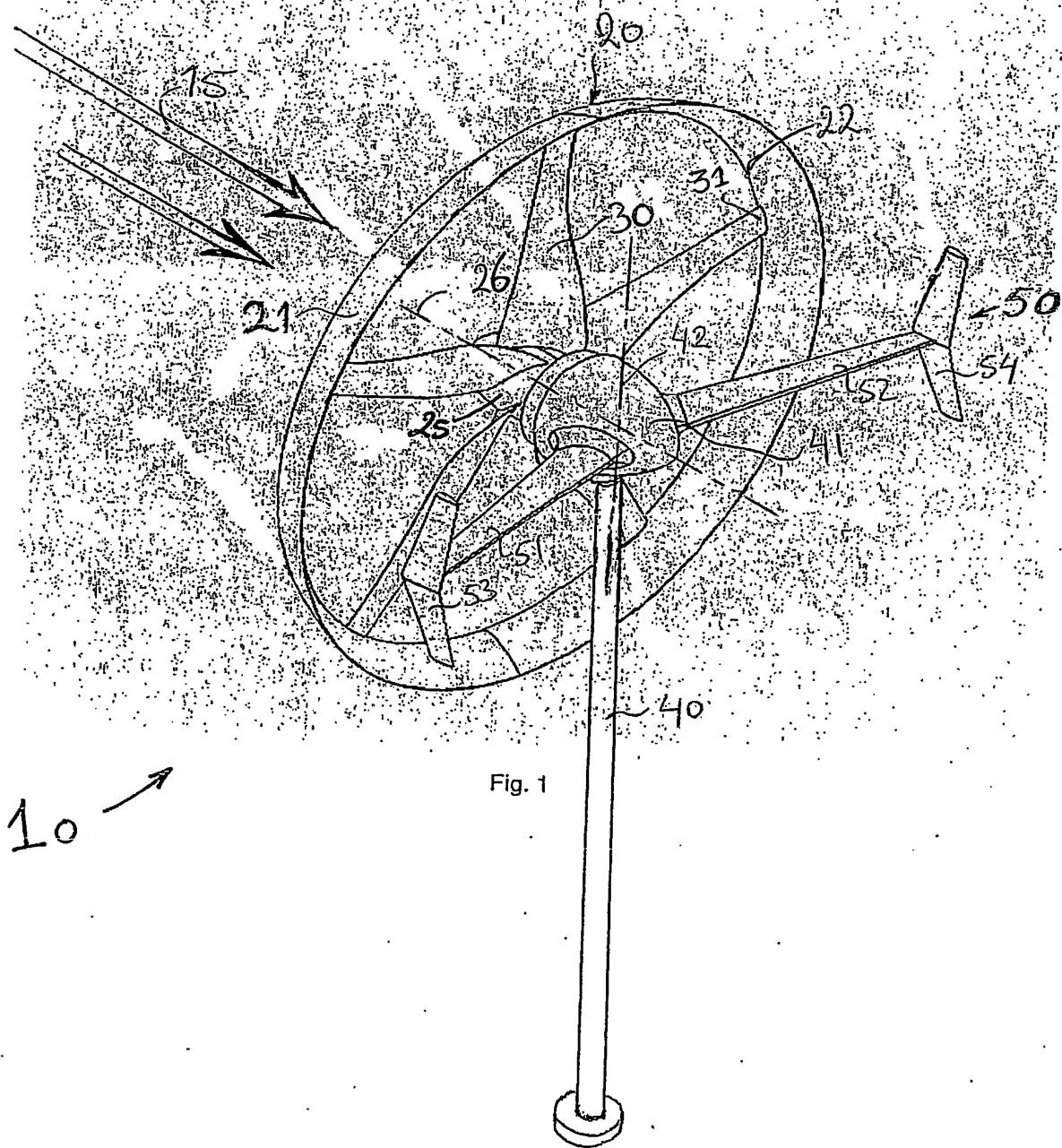


Fig. 1

10 →

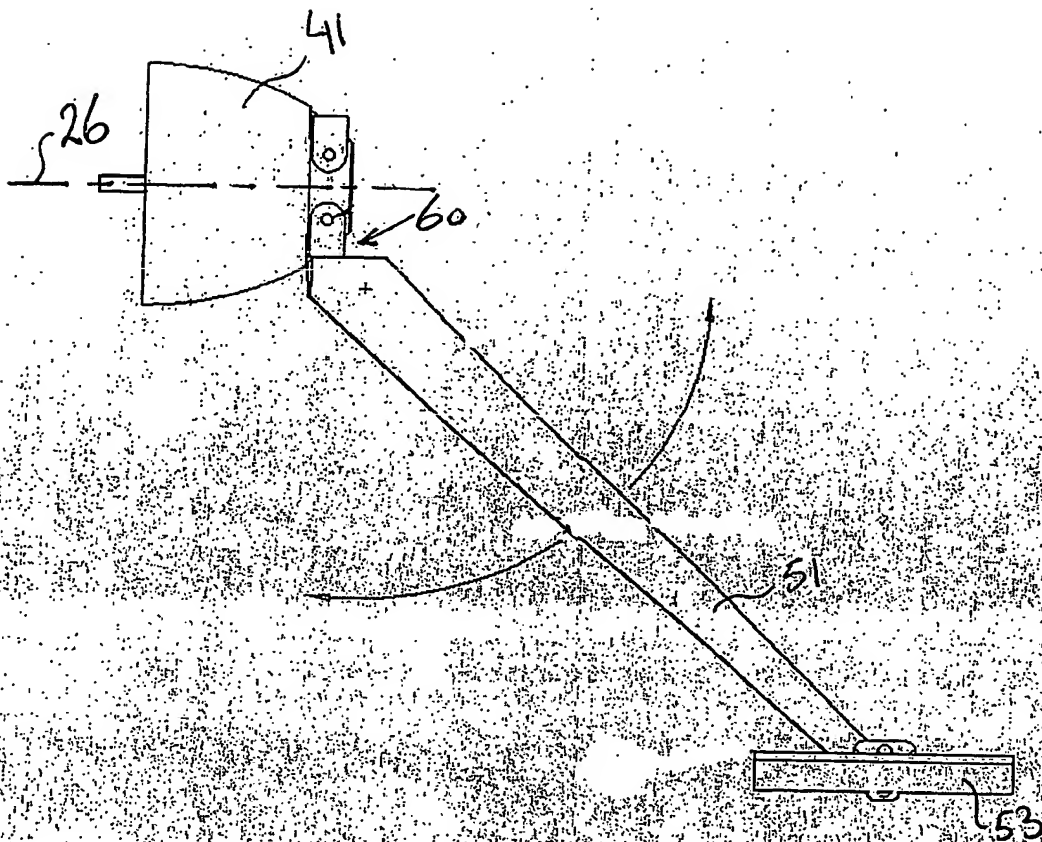


Fig. 3

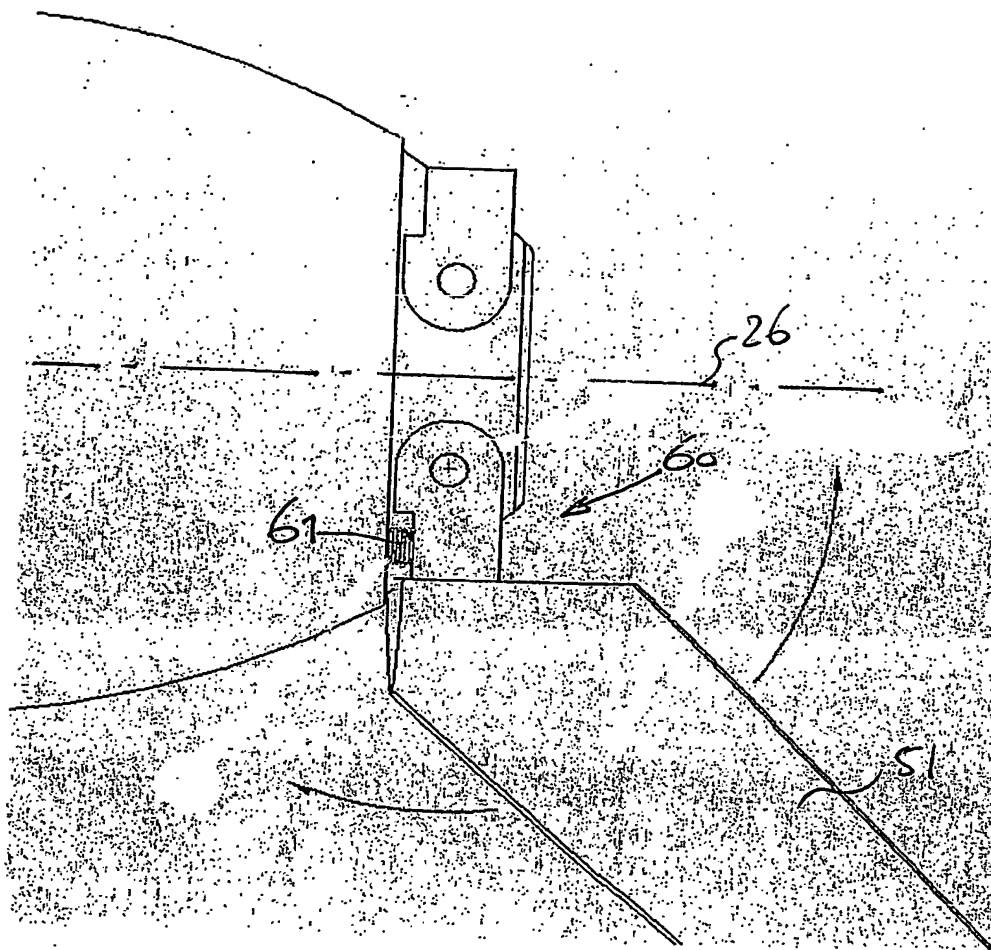


FIG. 4

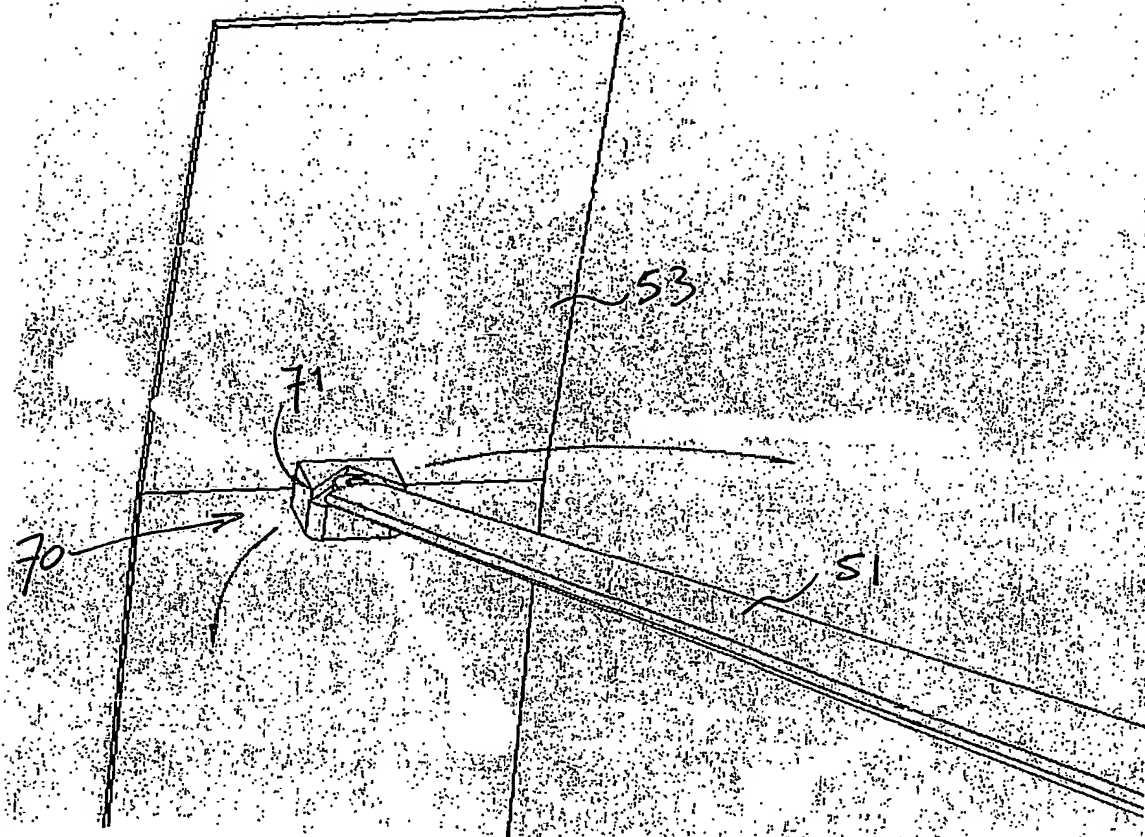


Fig. 5

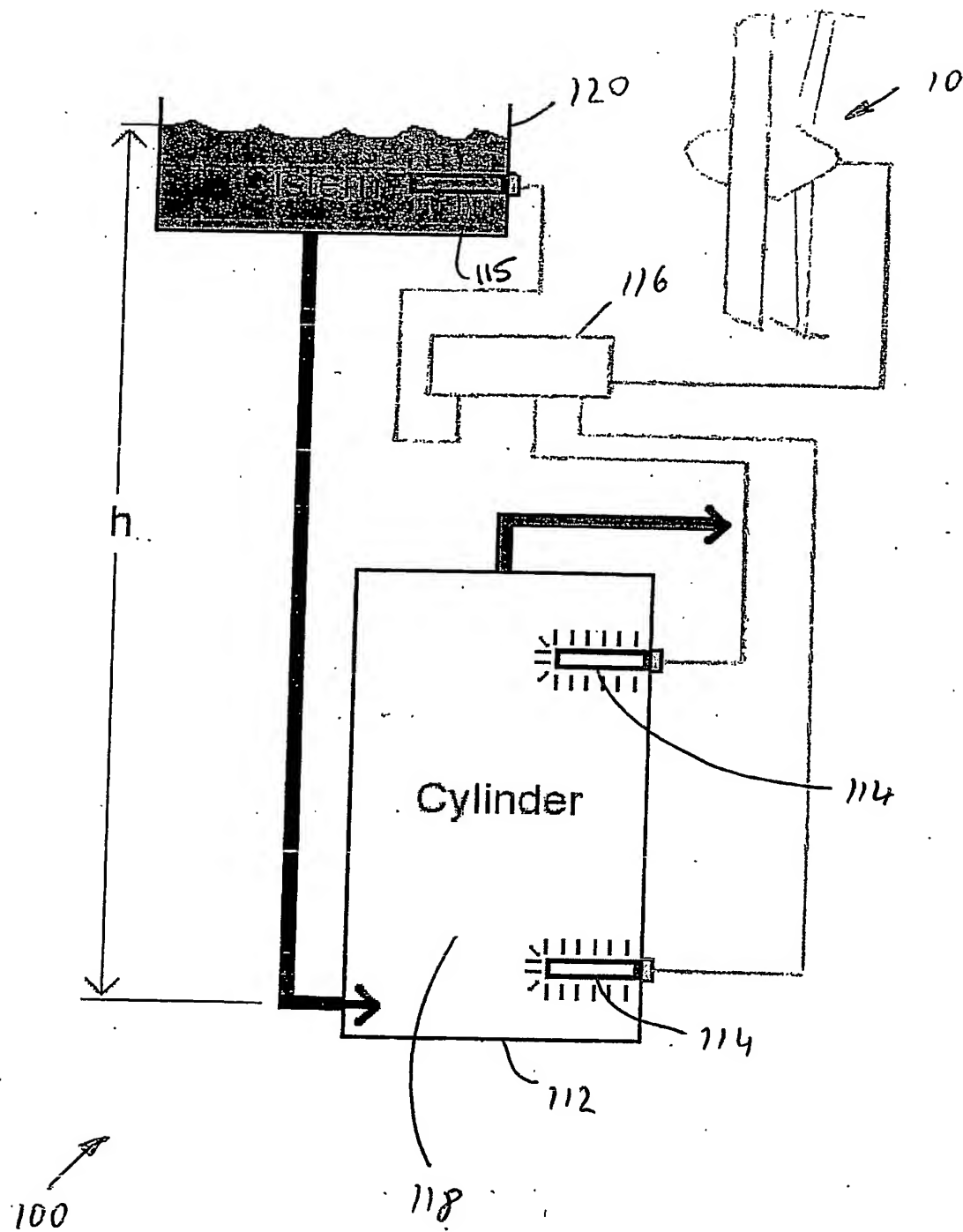


FIG. 6

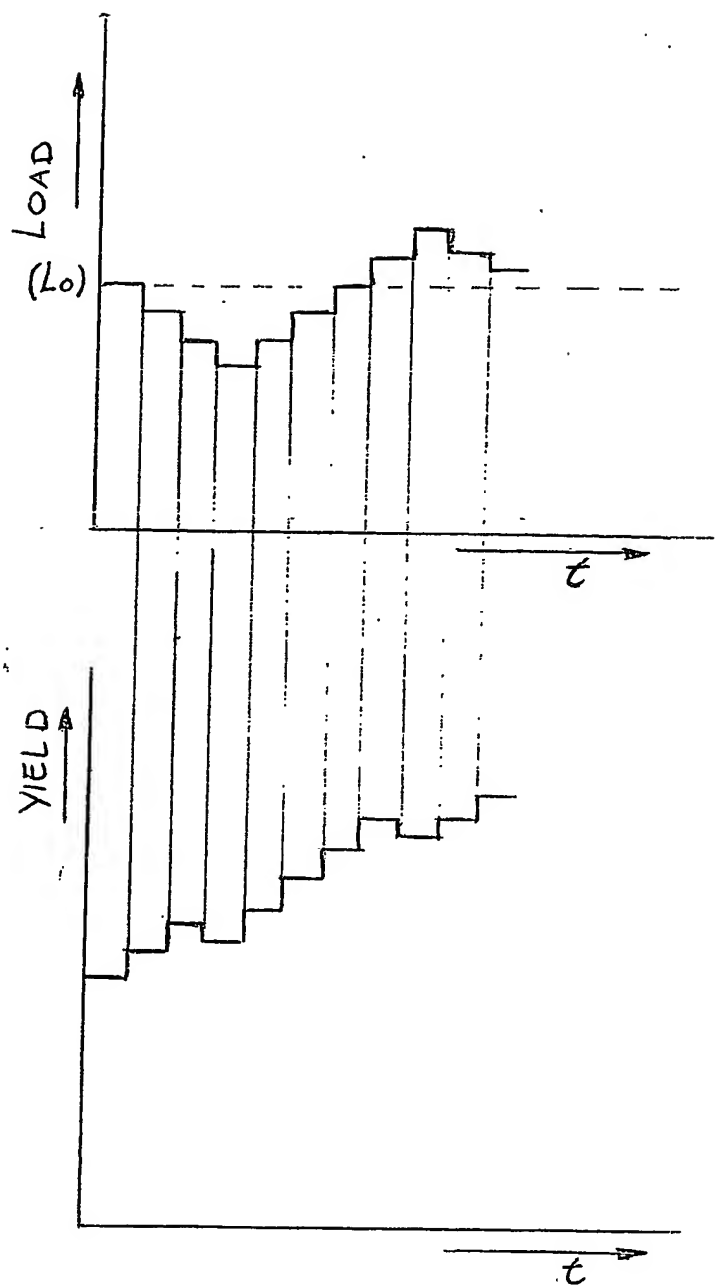


FIG. 7

FIG. 8.

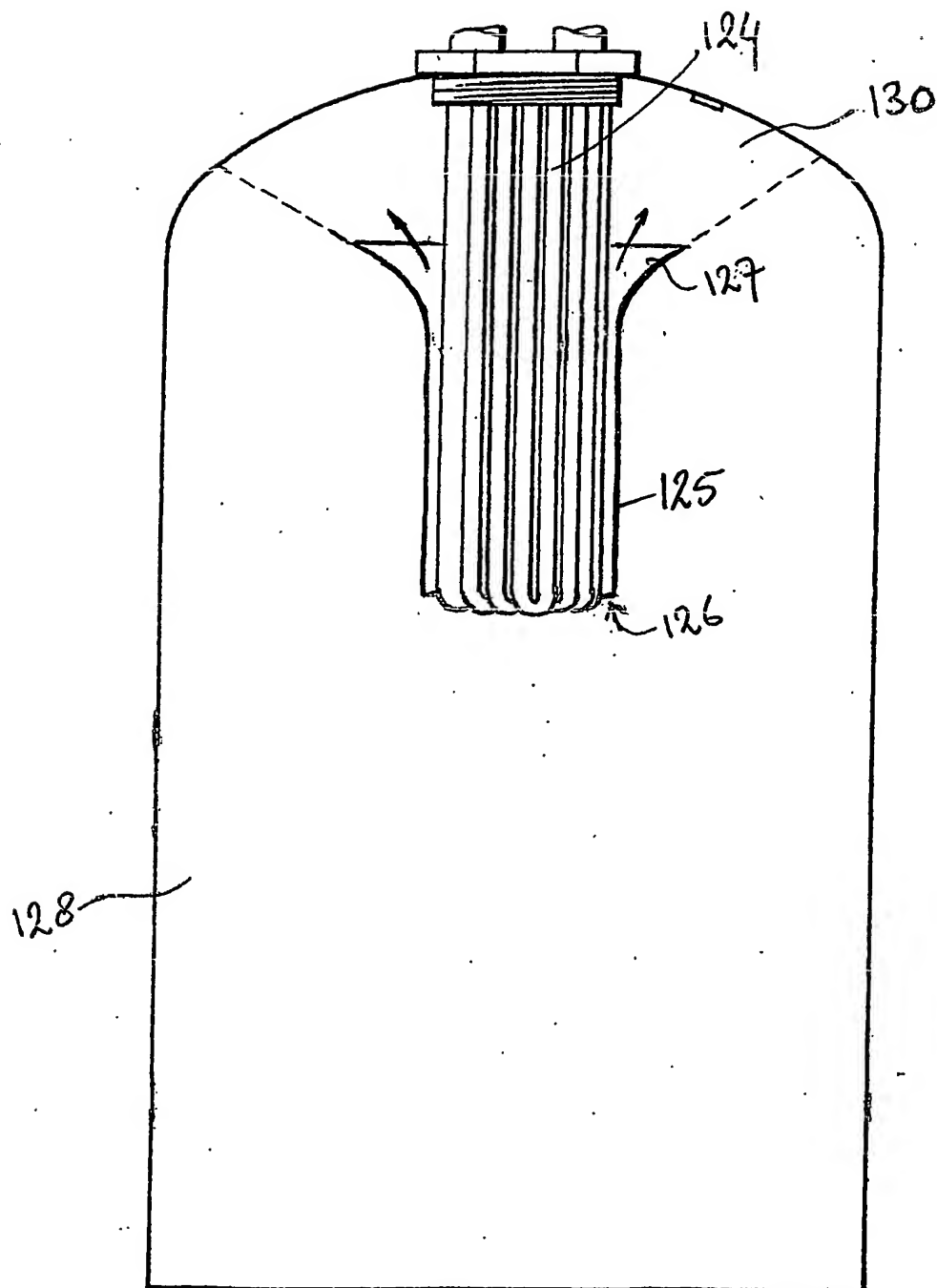
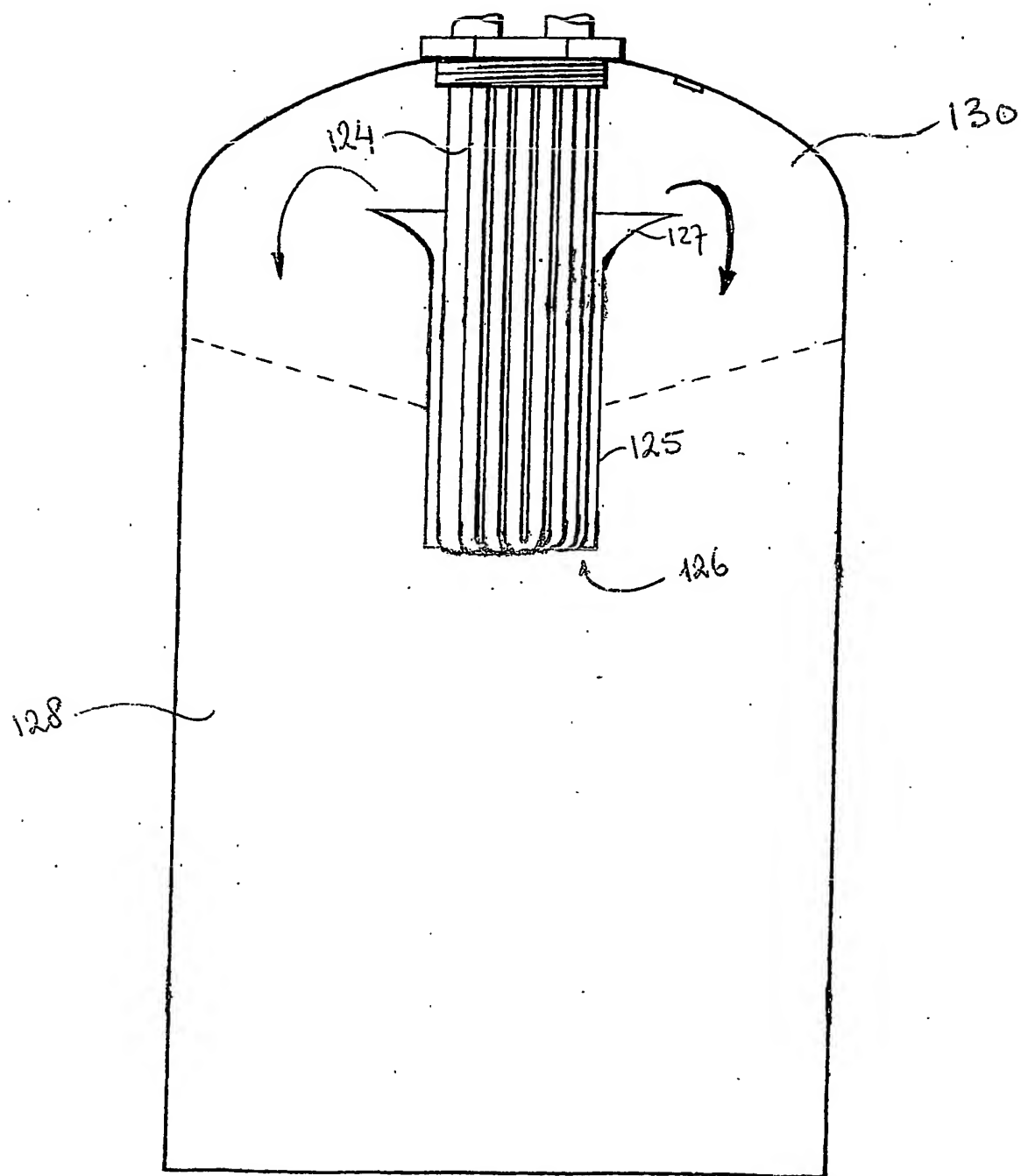


FIG. 9



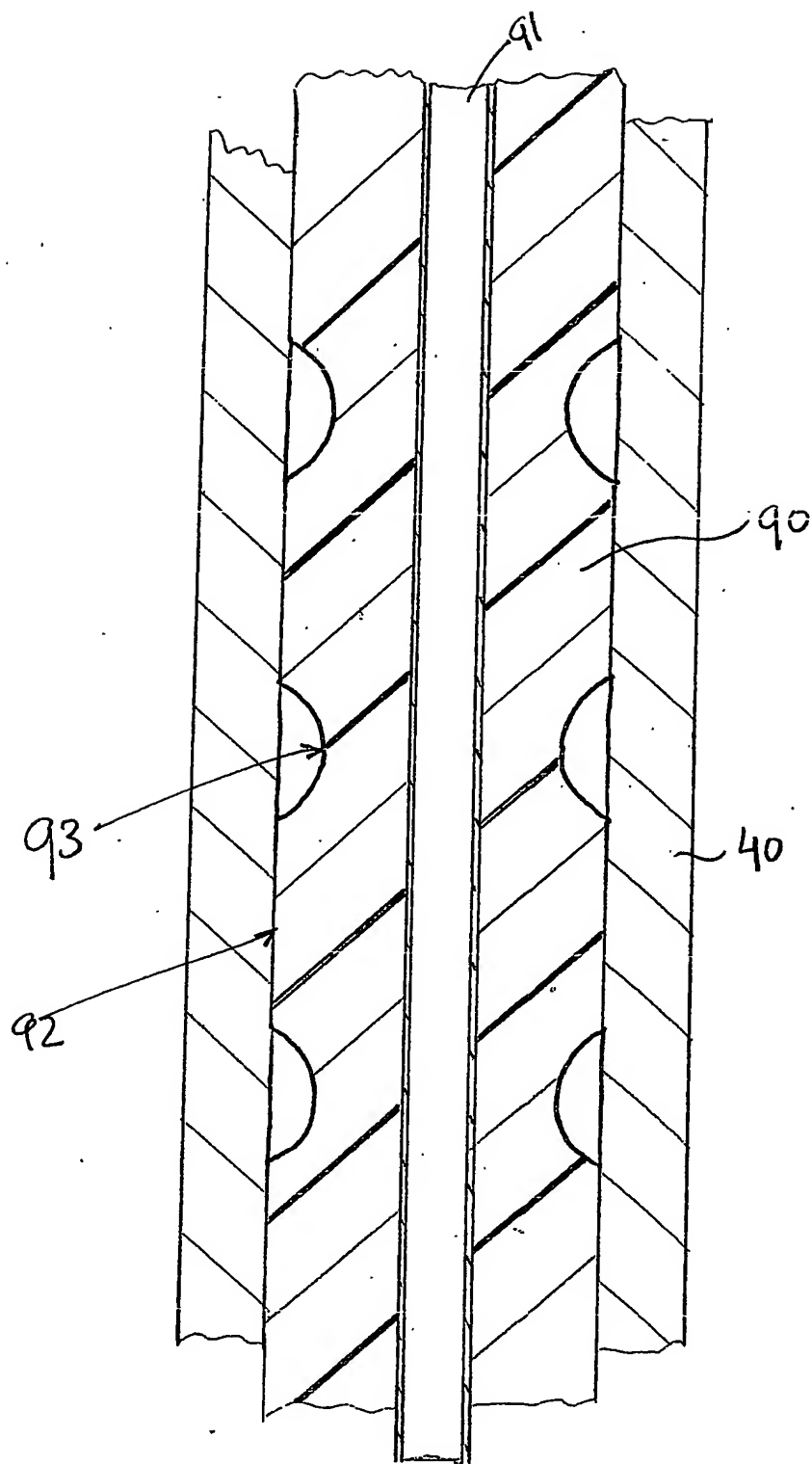


FIG. 10

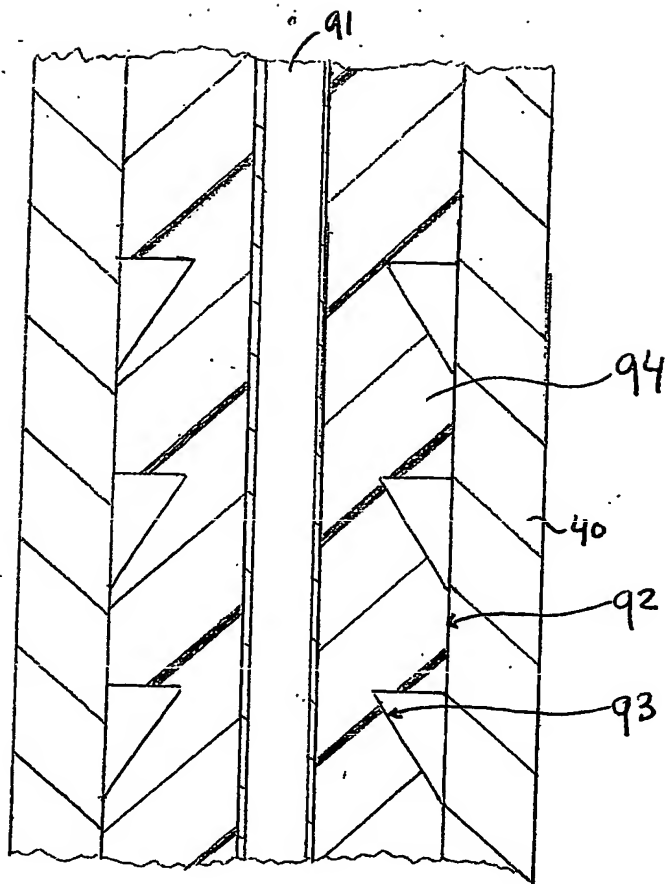


FIG. 11

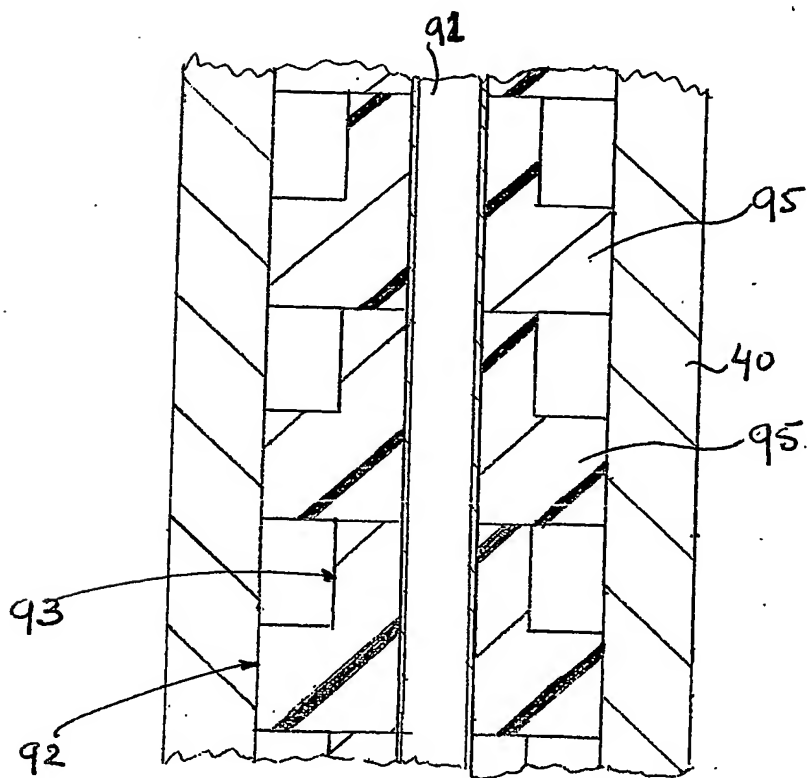


FIG. 12



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